

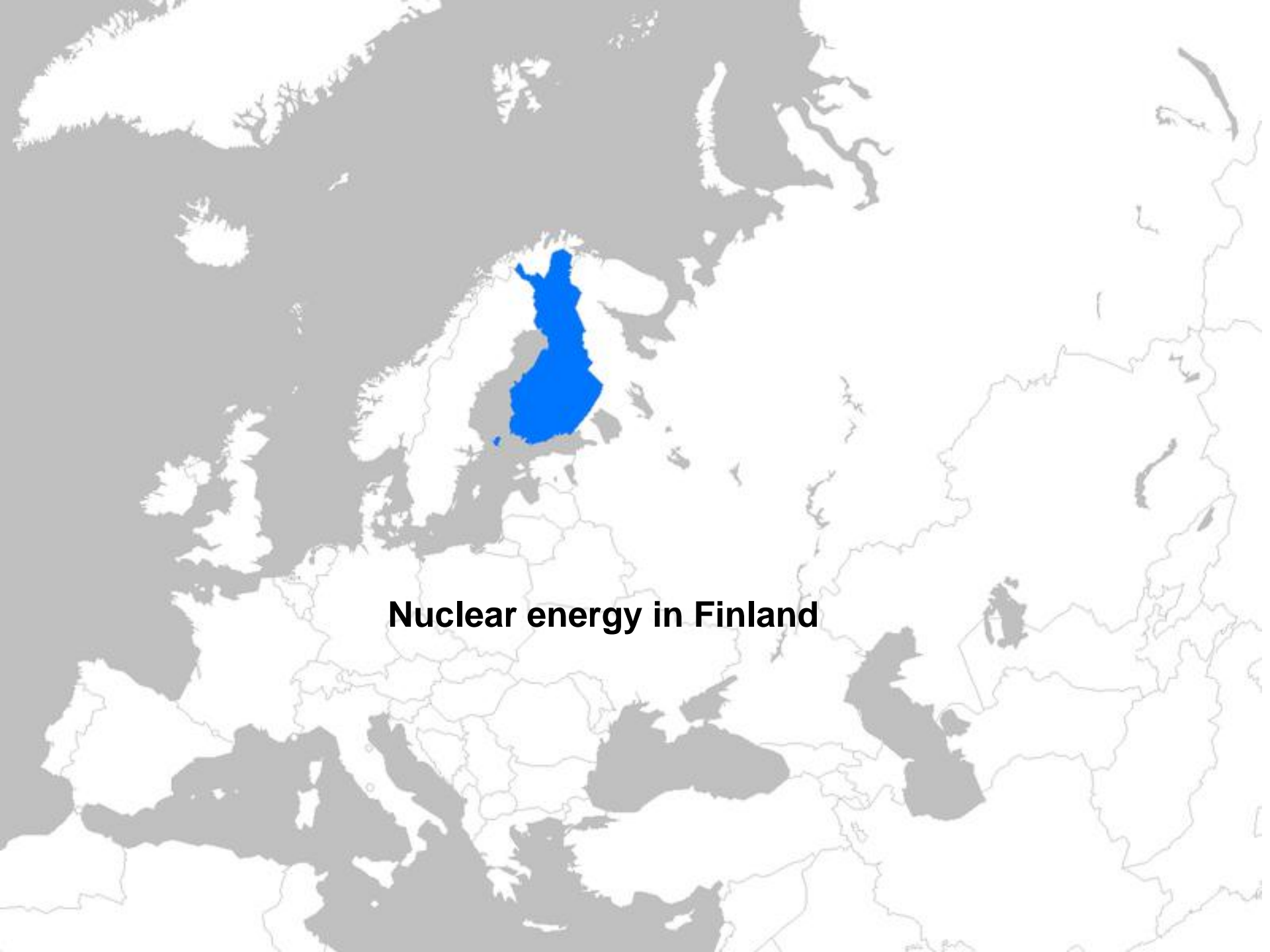
# ISSUES ON APPLICATION OF COMMERCIAL LWR CORE AREAS FOR IRRADIATION AND FOR TESTING OF ADVANCED FUELS

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1. Introduction – Nuclear energy in Finland
2. Why and how thorium in Finland
3. Reactor physics of Th fuel assemblies in LWRs
4. Conclusions



**Nuclear energy in Finland**

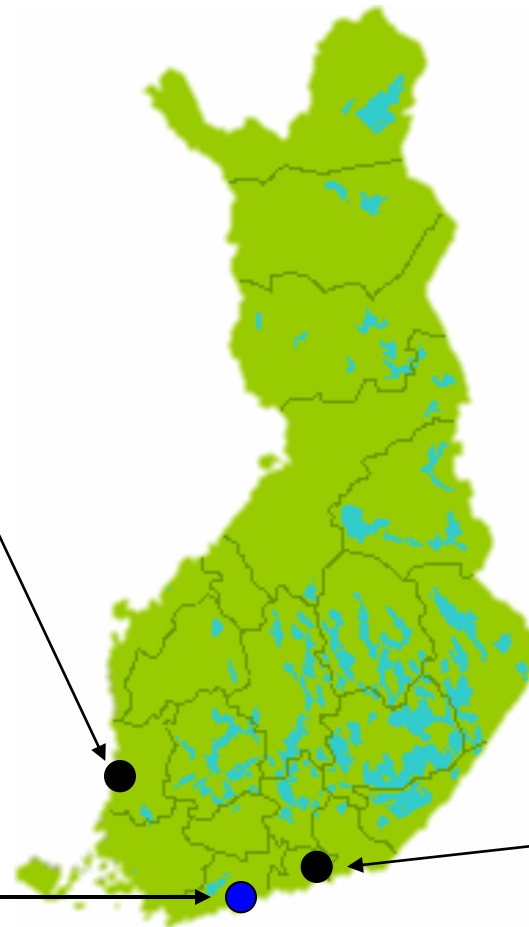
# 25,4% of electricity by nuclear (2008)



Olkiluoto 1&2  
BWR 880&860MW  
1979, 1982  
2008: 14.4TWh, 95%



Loviisa 1&2  
PWR 2×488MW  
1977, 1981  
2008: 7,7TWh, 90%



Triga MkII  
1962, Espoo

Helsinki

# The 5th unit under construction Commercial start in 2013

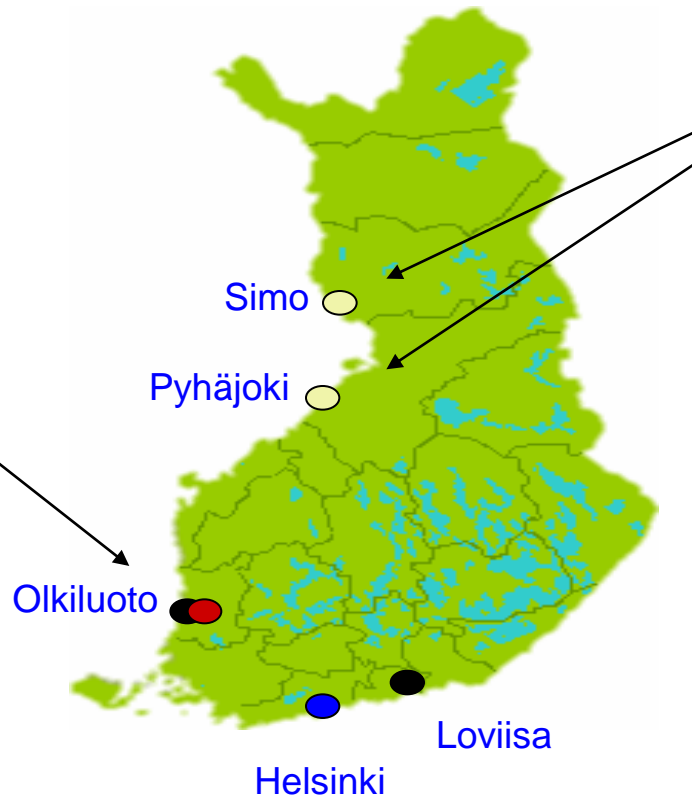
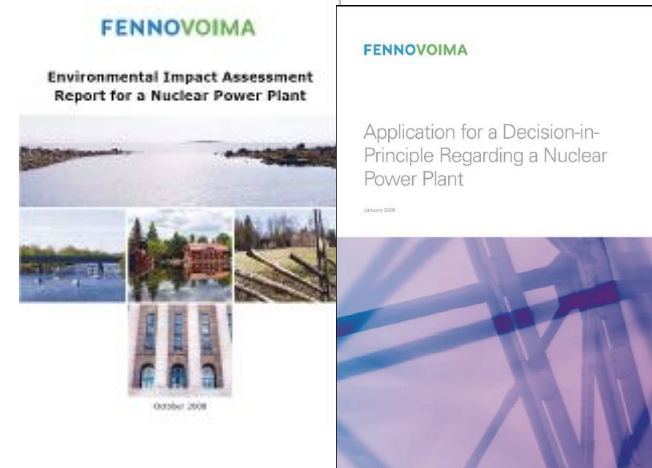


# Environmental Impact Assessments and Applications for Decision in Principle accepted for two further units

TVO, Olkiluoto 4



Fennovoima 1



Commercial operation by 2020  
Fennovoima site selection  
Waste management of Fe1  
Five reactor candidates in DiP  
Consequences of EU stress tests  
DiP assumes sufficient know-how

[www.tem.fi](http://www.tem.fi)

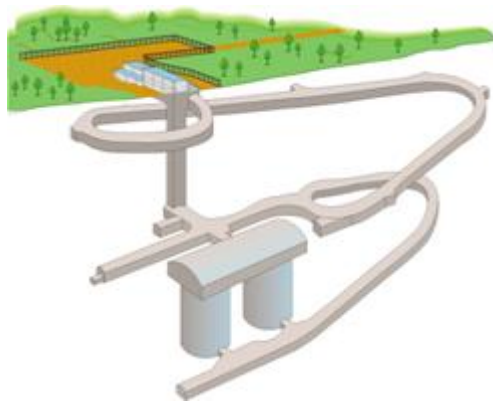
Ministry of Employment and the Economy

# Nuclear waste management in Finland

## Olkiluoto Power Plant



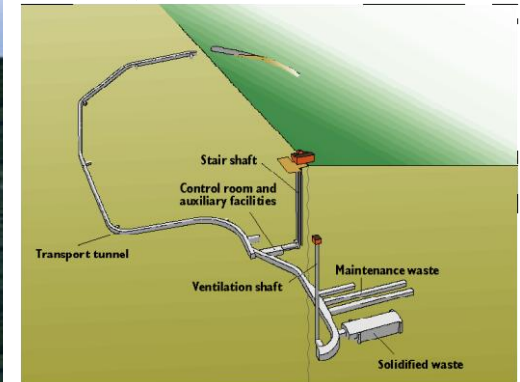
Operational waste  
TVO



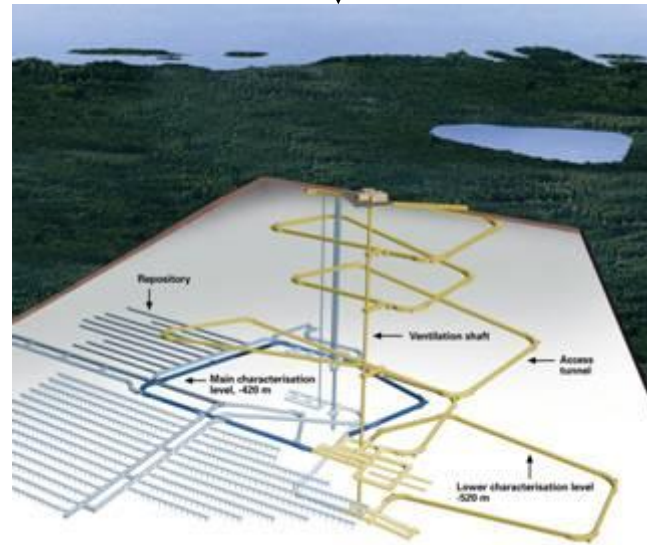
## Loviisa Power Plant



Operational waste  
Fortum

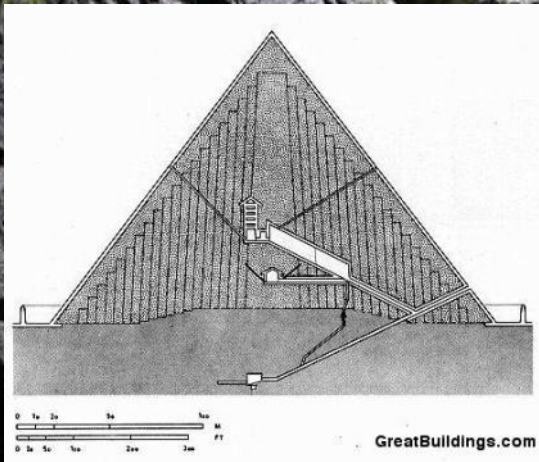


Spent fuel  
Posiva



[www.posiva.fi](http://www.posiva.fi)

Construction license in 2012, disposal start in 2020



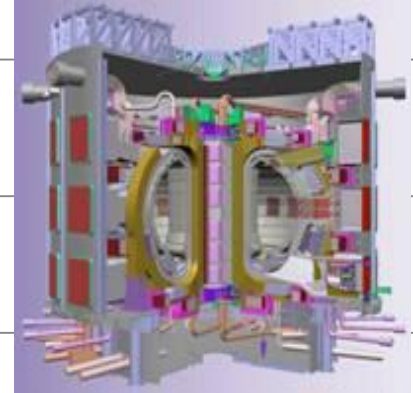
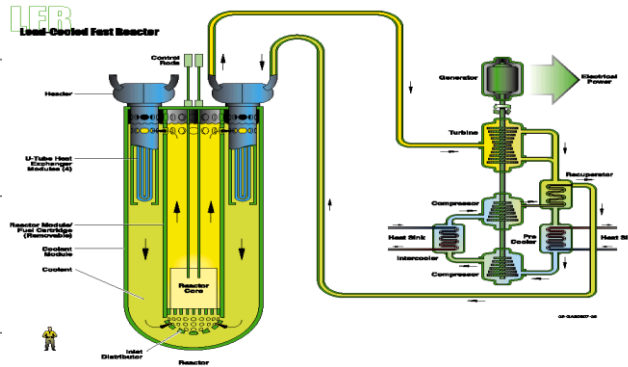
Posiva Oy/ Jussi Partanen

# Energy R&D involves long-time commitment – there is time for emerging systems

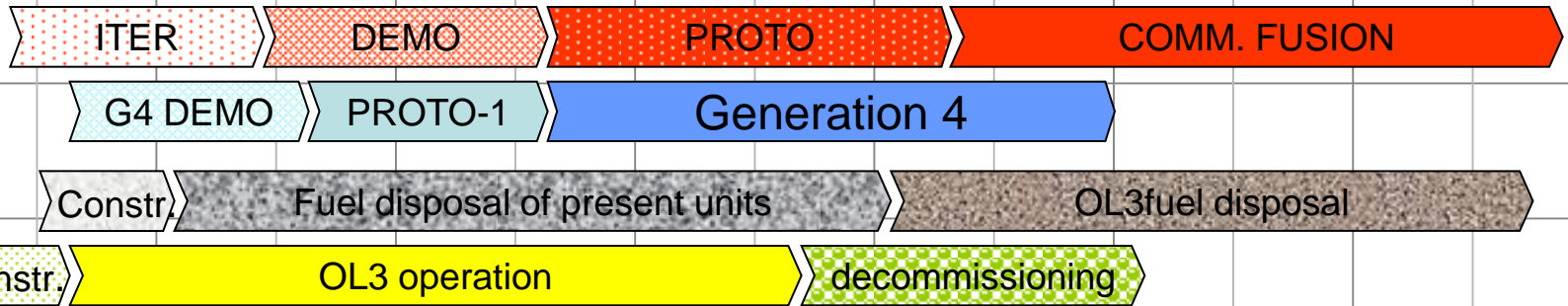


Generation 4

Generation 5



Generation 3



2000

2020

2040

2060

2080

2100

2120

2140

## Why and how thorium in Finland



Thor from Norse mythology  
Iceland,, 10th century

# Thorium as nuclear fuel – pros and cons

- **Sustainability:** Th adds significantly to U resources; abundant for breeders. Optimization between  $^{239}\text{Pu}$  and  $^{233}\text{U}$  cycles.
- **Safety 1:** Fuel – neutronics, thermal and chemical properties, burnup 100 MWd/kg, cladding performance, reactivity changes ( $^{233}\text{Pa} \rightarrow ^{233}\text{U}$  accumulation, burnable poison, B-shim)
- **Safety 2:** Reactor dynamics (thermal or fast, heat transport), full Th-usage with cycle different stages from  $^{239}\text{Pu}$  to  $^{233}\text{U}$  (life-cycle assessment). Decay heat for both shut-down and for intermediate fuel disposal.
- **Nuclear waste:** fission products vs. actinides. Is P&T practicable?
- **Safeguarding:**  $^{232}\text{U}$  a radiation barrier,  $^{232}\text{Pu}$  production, seed enrichment LEU
- **Thorium technology:** fuel, reprocessing, reactor, O&M. A new NPP design is needed. Small nuclear countries have to rely on international markets.
- **Economic viability:** price of  $^{235}\text{U}$ ? BOC and EOC views  
Very different opinions.



**For the near future Th is not a bargain?**

# Th-fuel: Motivation and challenges regarding Finland

- Th-U –fuel in **present LWRs**. A small nuclear country cannot afford prototypes.
- **Once-thru cycle**: wasting fissile material?
- **Reprocessing** in an international facility; transport of active fuel assemblies.
- Modifications of **waste management** concepts, vitrified waste
- Licensing of Th fuel in LWRs
- **Cost** structure of nuclear energy in Finland; viability of Th, competition against MOX and price of Pu. Comparisons between OL3 and a AHWR. Th almost free, U about 45% of the fuel costs
- **Short-term benefits** arise from spin-offs, education, code-validation in new parameter ranges, etc



A.Gallen –Kallela, Forging of the Sampo, 1893



A.Gallen –Kallela, Defence of the Sampo, 1896  
**Sampo, a magical artifact that produced good fortune to its holder**

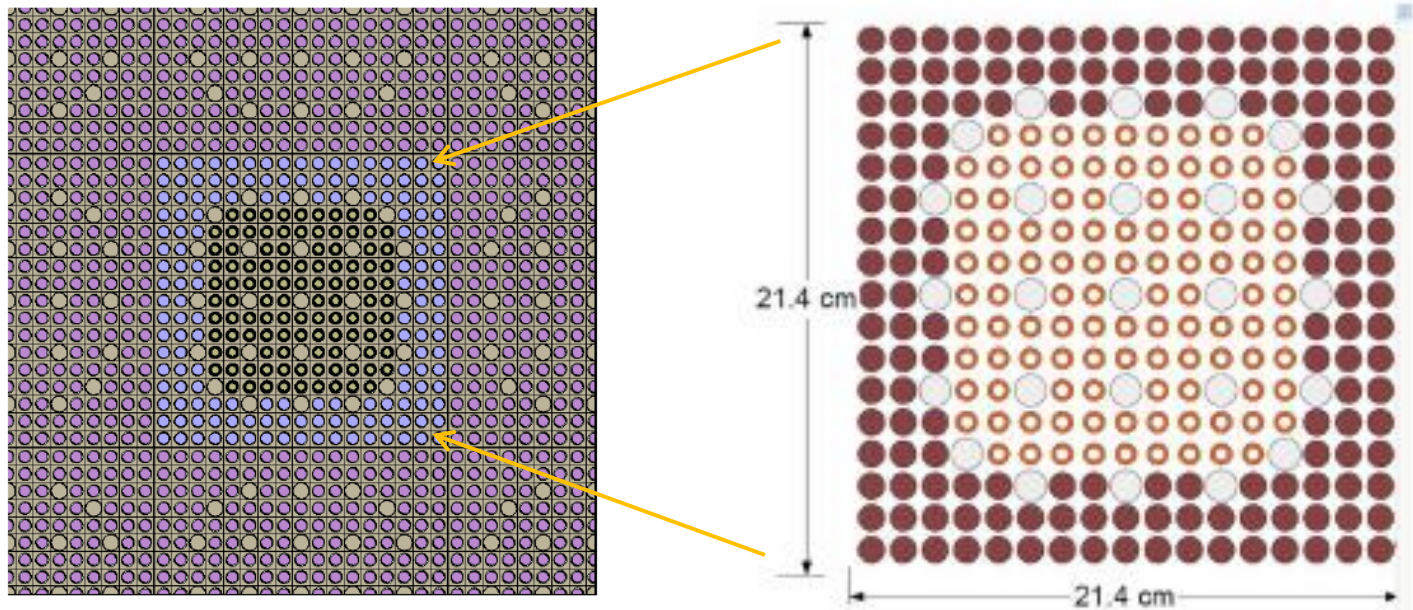
## Thorium assemblies in present LWRs

# Code calculations

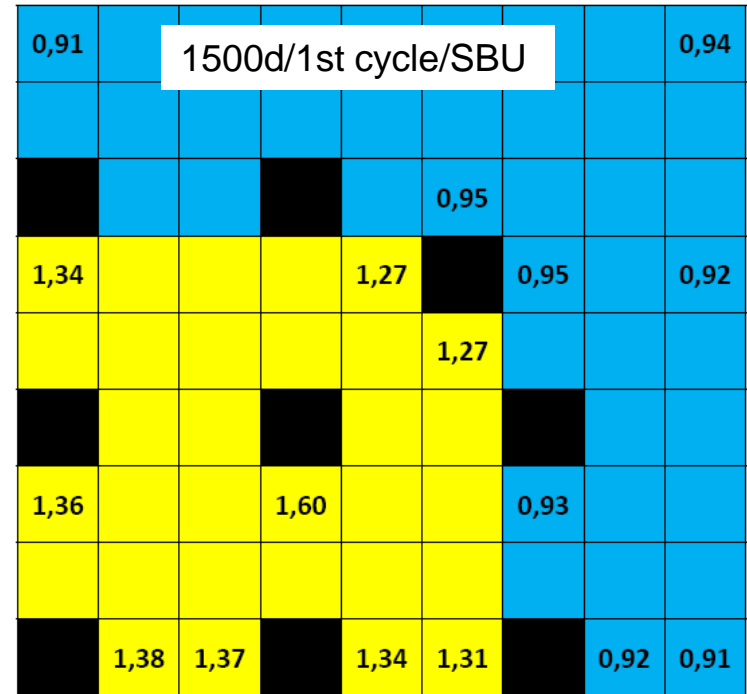
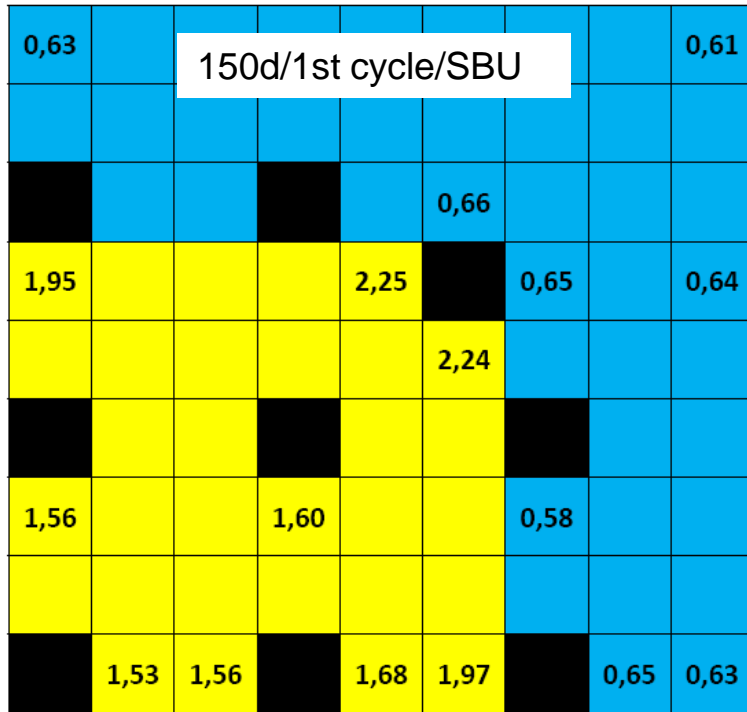
- Academic problems with professional tools. Monte Carlo Codes MCNP, Serpent, FLUKA, and burnup codes CASMO, Serpent, MonteBurns, DeTra
- Educational goals
- Benefits for code development and validation
- A soft transition from present generation systems into a fully new fuel structure: Th contained in single rods, fuel assemblies, and full core loads
- **A single Radkowsky type seed blanket unit (SBU) in a PWR.** Comparison between Serpent and CASMO. Neutronics and burnup calculations.
- **Full Th-U core in a BWR.** Possibilities for 3D enrichment and spectral shifts. Core load optimization
- Miscellaneous comments on proliferation, spent nuclear waste
- Consideration of test rods for isotope separation and materials tests, licensing requirements

# Thorium in PWR

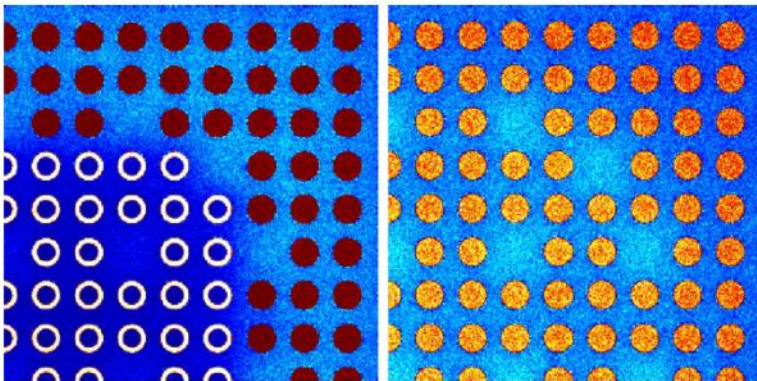
- Use of thorium fuel in a commercial PWR  $\text{UO}_2$  core (4% enriched)
- Performance of a single Radkowsky thorium fuel assembly : 17×17 Westinghouse PWR, separate blanket (BSA) and seed sub-assemblies (SSA); details as in Todosov and Kasimi (2004)
- Seed blanket changed in 54 month cycles
- Calculations by CASMO-4E and by a Monte Carlo code Serpent
- Role of soluble boron, typical values used here



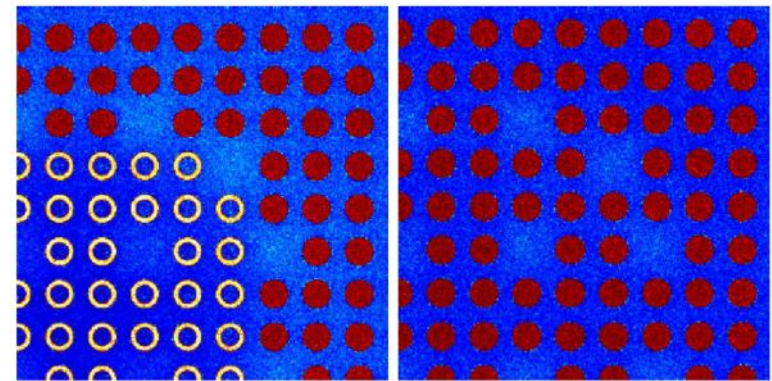
# Neutron flux and fission rate distribution



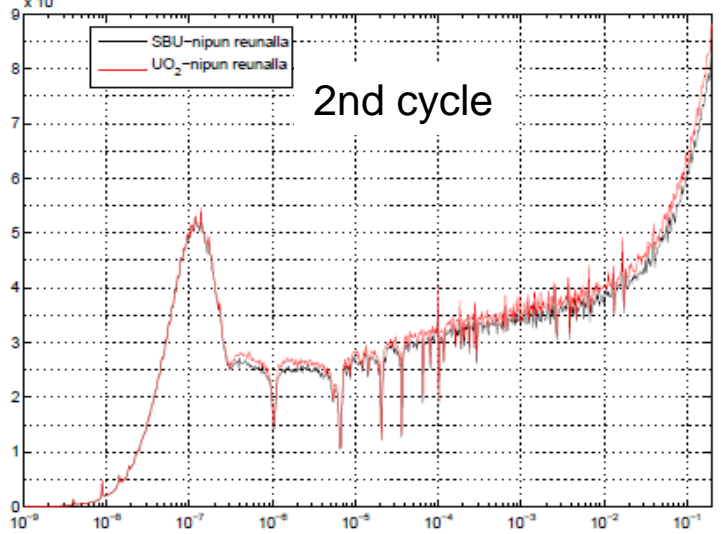
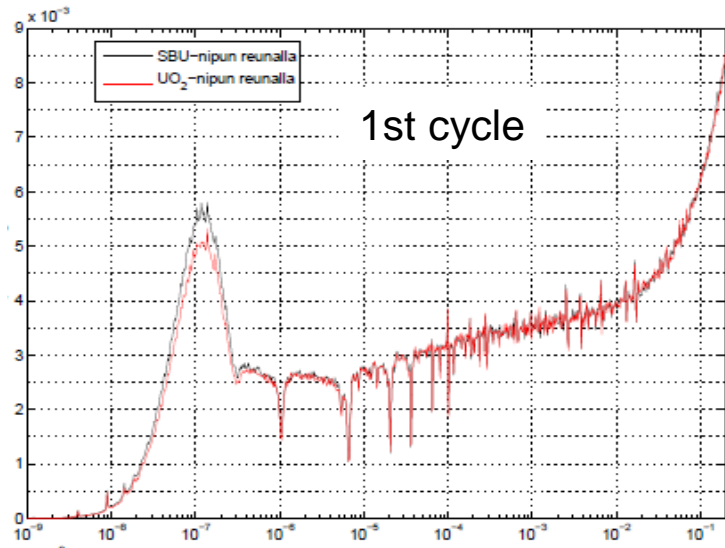
SBU



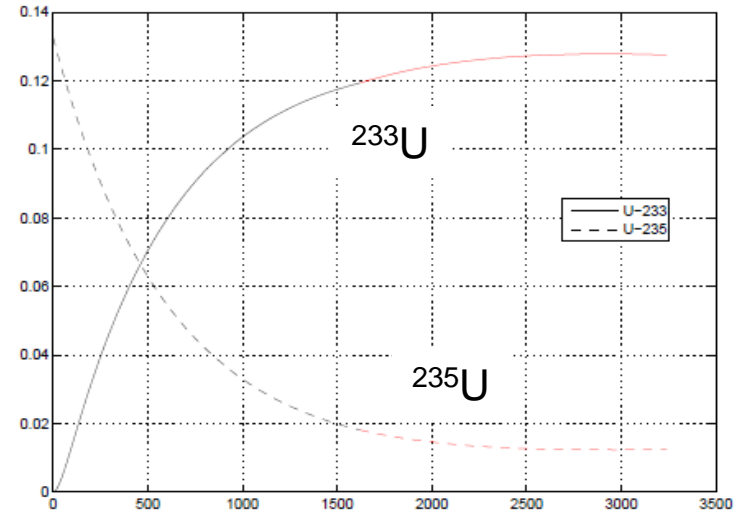
UO<sub>2</sub>



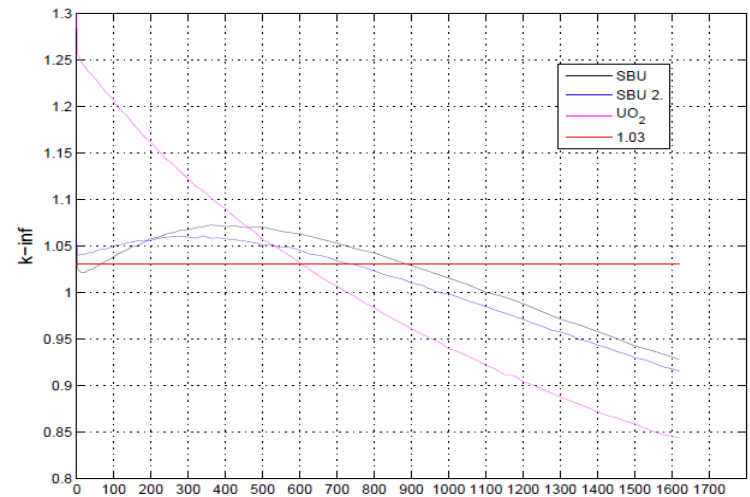
Neutron flux/lethargy at the SBU border (red) and in the UO<sub>2</sub> region (black)



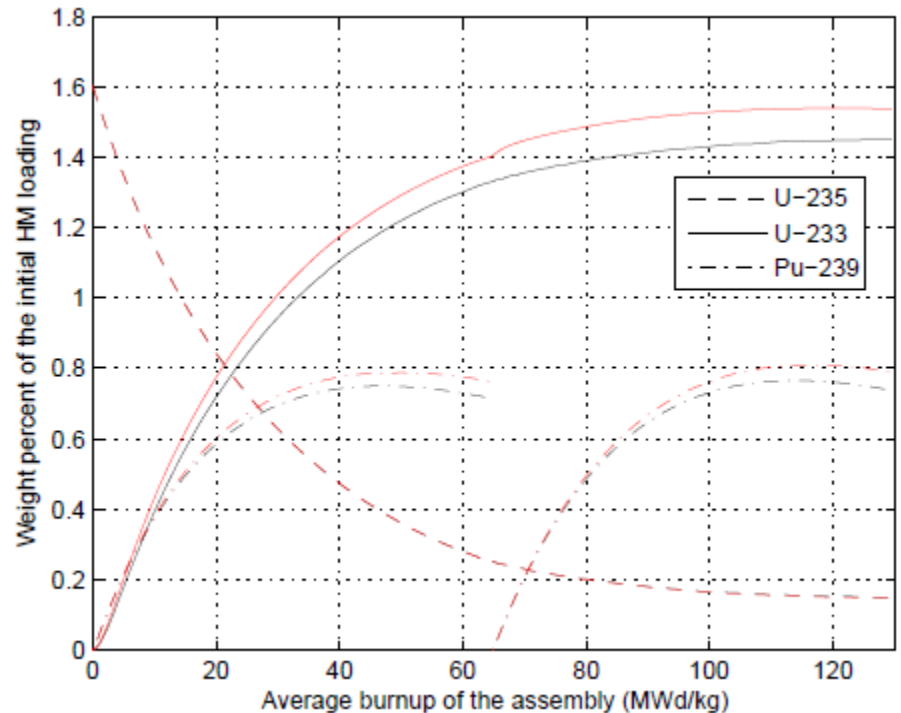
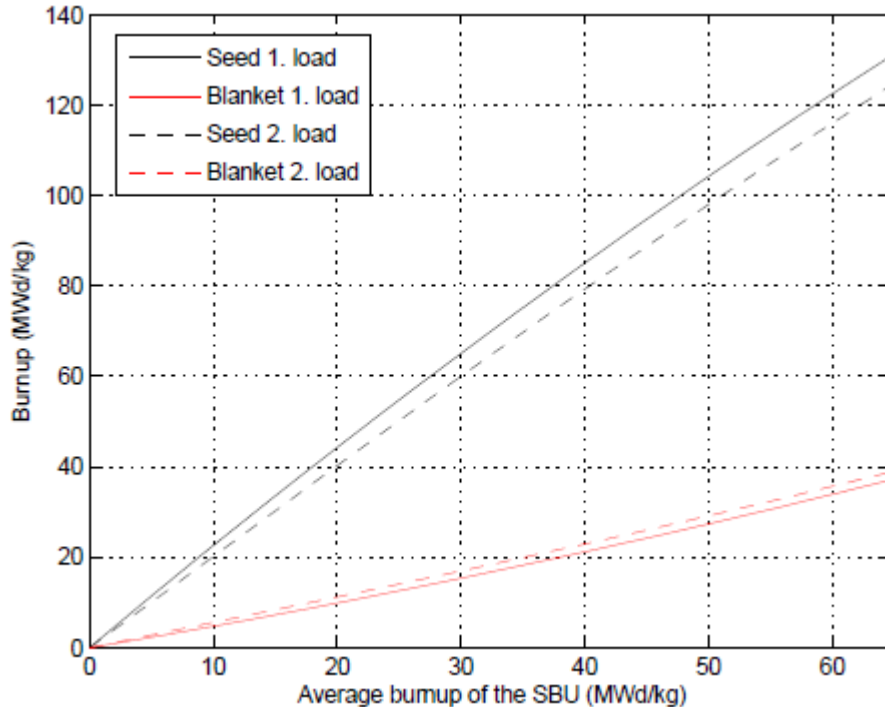
Fissile mass density (g/cm<sup>3</sup>) vs. time (d)



Multiplication factor vs. time (d)



# Burnup and fissile production

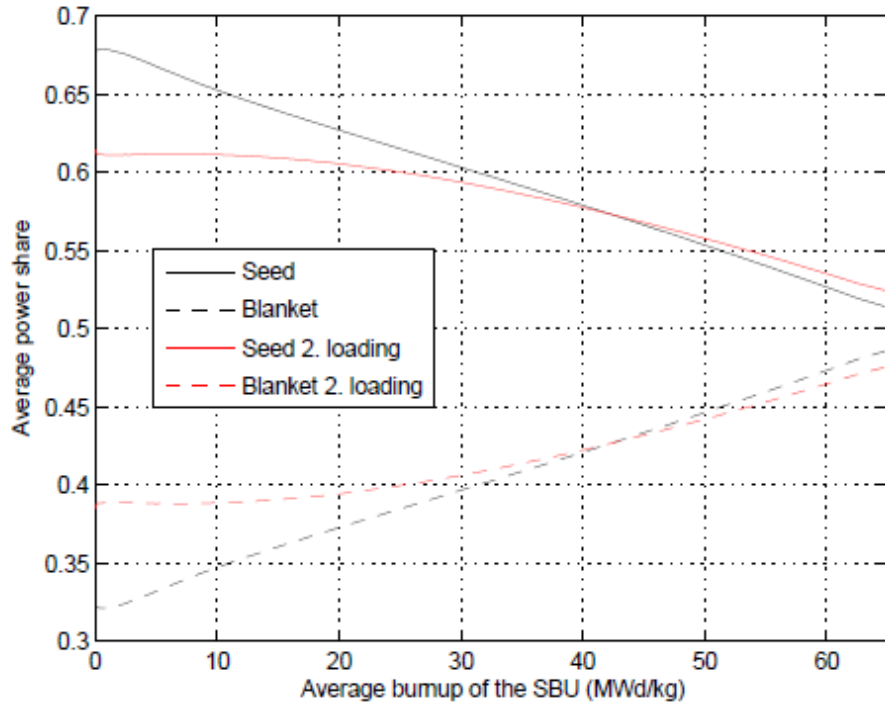


Burnup for a 54-month cycle. Discharge burnups (MWd/kg):

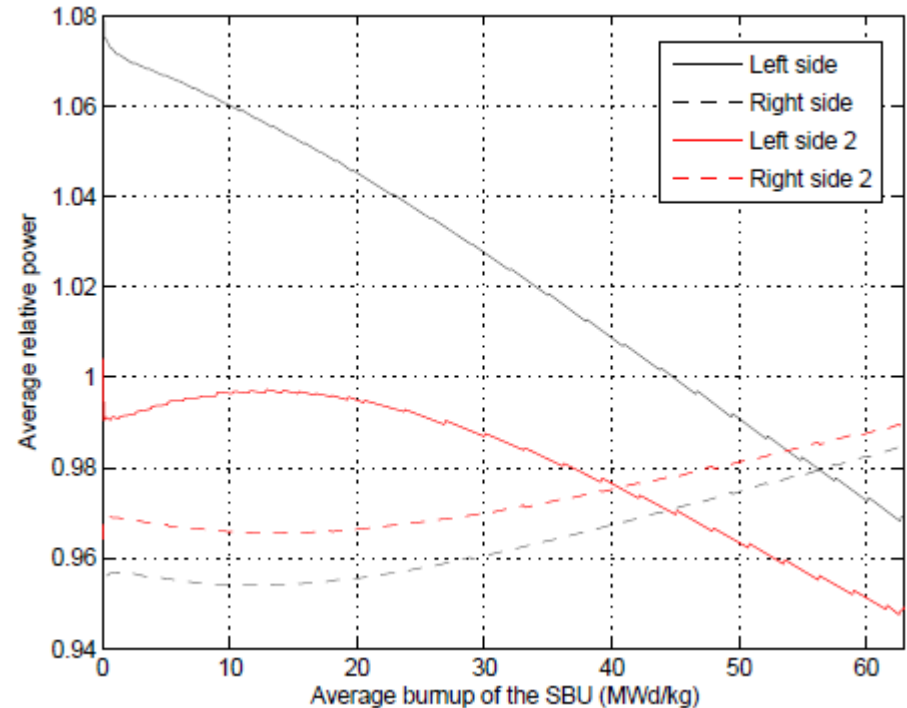
seed (1st cycle)	130.9	(129,5)
seed (2nd cycle)	124.4	(122,5)
blanket (1st cycle)	37.2	(37,7)
blanket (2nd cycle)	38.9	(39,7)
Casmo (Serpent)		

Serpent predicts slightly more  $U^{233}$  production than Casmo-4E; very little difference in  $U^{235}$  depletion

# Relative power production of RTF and LWR assy

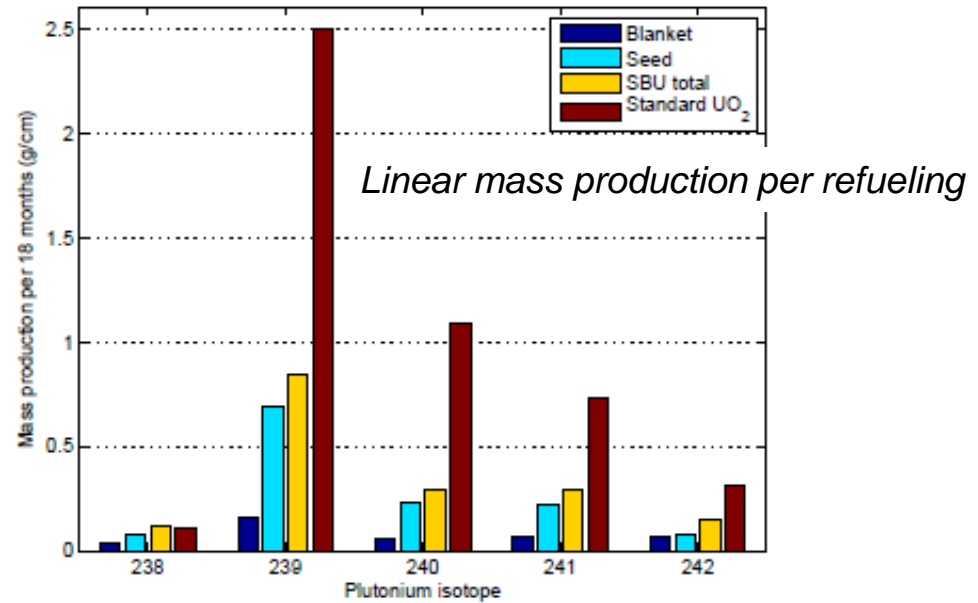
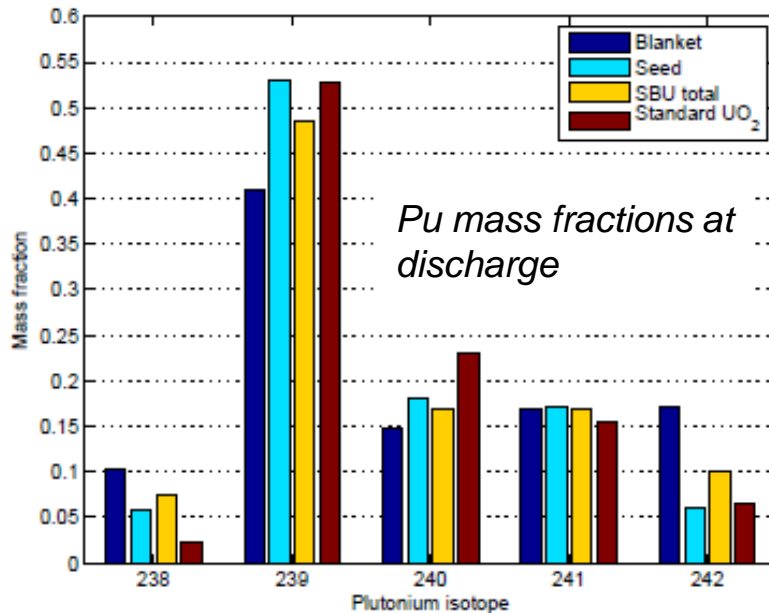


Relative power shares of the blanket and seed



Relative power shares of the left and right side of the UO<sub>2</sub> assembly next to SBU. Average relative power for assembly equals unity. Second cycle in red.

# Proliferation aspects



UO<sub>2</sub> discharge burnup is 45MWd/kg and that of SBU 64.8 MWd/kg. Spontaneous neutron rates 7.23, 4.46, and 4,12 (in 10<sup>5</sup>/kgs) of seed, Blanket, and UO<sub>2</sub>, respectively.

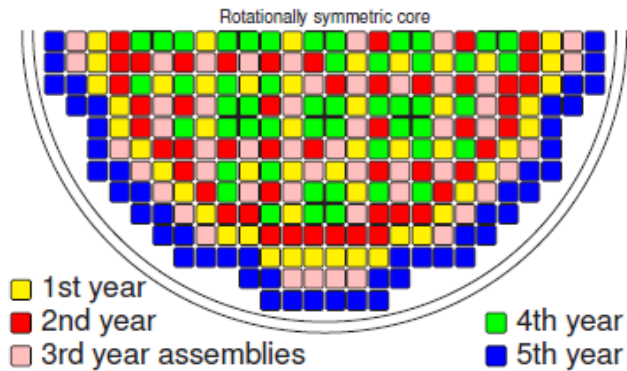
*Isotopic mass fractions of the discharged uranium*

Nuclide	Standard UO <sub>2</sub>	Seed	Blanket
U-232	0	0	0.0009
U-233	0	0	0.1201
U-234	0	0	0.0361
U-235	0.0089	0.0719	0.0123
U-236	0.0056	0.0307	0.0185
U-238	0.9855	0.8973	0.8121

# Full thorium fueled core in a BWR

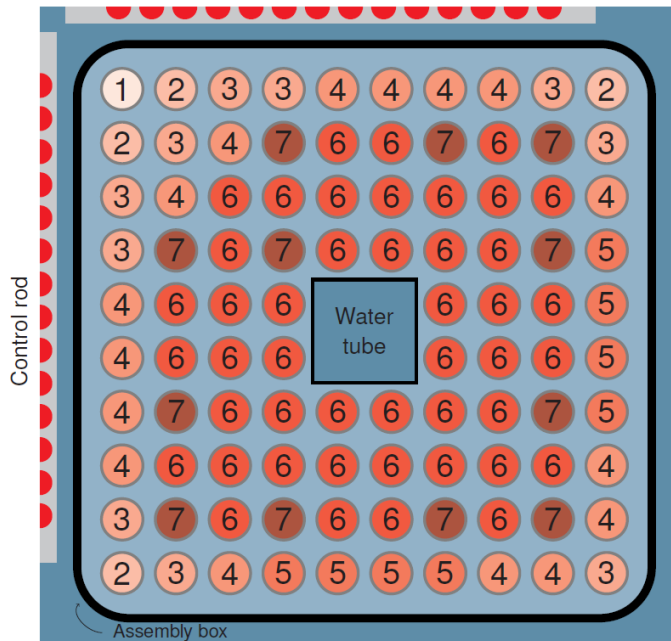
# Thorium simulation in a BWR

Core layout



- 1st year
- 2nd year
- 3rd year assemblies
- 4th year
- 5th year

Control rod



Specification

- ▶ Thermal power 2500MW
- ▶ Cycle 324 days
- ▶ Batches 5
- ▶ Number of assemblies 500
- ▶ B<sub>4</sub>C control rods
- ▶ Control using core flow and control cells

Specification

- ▶ 10 × 10 lattice, square water hole
- ▶ 15.375 cm × 15.375 cm × 3.68 m
- ▶ The lowest enrichment 1.7wt-% (pin 1)
- ▶ The highest enrichment 4.95wt-% (pin 6)
- ▶ Average enrichment 4.125wt-%
- ▶ Gadolinium content 4.0wt-% in pin 7
- ▶ Pin pitch 1.3 cm
- ▶ Pin diameter 1.0 cm
- ▶ Heavy metal content 492 g/cm
- ▶ Design burnup 44.6 MWd/kgHM
- ▶ Natural uranium sections at the ends; otherwise no axial variation

# An equivalent Th BWR core load

- Spectral changes due to burn-up and void distribution. In a BWR true 3D variation of nuclide compositions. Absorbable poisons (Gd) common.
- The same energy and neutron production during lifetime production
- Very hard task for core load optimization. Reference layout and control plan
- Casmo-4E was used for lattice calculations
- Simulate-3 for full core calculations

## Thorium design #1

- ▶ Enrichments proportional reference assembly
- ▶ Average enrichment 5.34wt-%
- ▶ Uranium enrichment 12.88wt-%
- ▶ Balance thorium
- ▶ Heavy metal content 467 g/cm
- ▶ Design burnup 47.2 MWd/kgHM

## Thorium design #2

- ▶ Enrichments proportional to reference assembly
- ▶ Average enrichment 5.10wt-%
- ▶ Uranium enrichment 12.33wt-%
- ▶ Balance thorium
- ▶ Gadolinium content 3.0wt-% in pin 7
- ▶ Heavy metal content 467 g/cm
- ▶ Design burnup 47.1 MWd/kgHM

## Thorium design #3

- ▶ 12 × 12 assembly layout with 3 × 3 water hole
- ▶ Average enrichment 5.14wt-%
- ▶ Uranium enrichment 12.30wt-%
- ▶ Balance thorium
- ▶ Pin diameter 0.83 cm
- ▶ Pin pitch 1.11 cm
- ▶ Heavy metal content 421 g/cm
- ▶ Design burnup 52.3 MWd/kgHM

# Th in BWR – some preliminary findings

## Assembly performance

	Reference	Thorium #1	Thorium #2	Thorium #3
Local power peaking	1.232	1.258	1.244	1.229
Reactivity feedbacks	> 0 and < 0	< 0	< 0	< 0
Burnup at maximum reactivity (MWd/kgHM)	10.0	12.0	10.0	10.0

## Core performance

	Reference	Thorium #1	Thorium #2	Thorium #3
Maximum assembly axial power peaking	1.36	1.50	1.43	1.36
Maximum assembly radial power peaking	1.49	1.47	1.44	1.42
Maximum pin power peaking	2.48	2.49	2.34	2.16

- Th fuel needs less Gd (higher thermal absorption and conversion)
- Power peaking reduced
- Th fuel requires more fissile nuclides and SWU
- No optimization done, yet

# Conclusions

- Nuclear energy means a very long time commitment
- Safe and economic production of nuclear energy implies intensive efforts on R&D&D and E&T involving also many emerging concepts.
- Thorium fuel cycle provides interesting possibilities for a soft introduction of it even in current LWRs.
- PWR options with Radkowsky SBU appears feasible
- BWR core optimisation not yet done
- Th SBUs seem to be licensable
- The benefits like waste, proliferation, etc., of Th-cycle have been demonstrated
- Th economy and sustainability require international reprocessing facilities
- To obtain full benefits of Th-cycle would imply a complete redesign of the whole system of the nuclear energy structure.



Thank You!

Acknowledgements to Fortum, TVO and Academy of Finland